# 

# **TRAFFIC IMPACT**

# **ANALYSIS**

FOR

# **TERRAVITA**

LOCATED

IN

# **KNIGHTDALE, NC**

Prepared For:

Terravita Development, LLC 933 Old Knight Road Knightdale, NC 27545

NOVEMBER 2024

DRMP Project No. 24682

Prepared By: <u>CDS</u>

Reviewed By: <u>CTS</u>





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11/13/24

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> **Prepared By:** DRMP, Inc. License #F-1524

## TRAFFIC IMPACT ANALYSIS TERRAVITA

#### Knightdale, North Carolina

#### EXECUTIVE SUMMARY

#### 1. Development Overview

A Traffic Impact Analysis (TIA) was conducted for the proposed Terravita development in accordance with the Knightdale (Town) Unified Development Ordinance (UDO) and North Carolina Department of Transportation (NCDOT) capacity analysis guidelines. The proposed Terravita development is to be located south of Buffaloe Road between Quiet Oaks Drive and Bobbitt Drive in Knightdale, North Carolina. The proposed development, anticipated to be completed in 2029, is assumed to consist of 170 single-family lots and 75 townhomes. Access to the parcel is proposed via one full movement driveway along Buffaloe Road and internal connections to Quiet Oaks Road, Bobbitt Drive, Proc Ridge Lane, and the Old Knight Road extension (a part of the Weldon Village adjacent development).

#### 2. Existing Traffic Conditions

The study area for the TIA was determined through coordination with the Town and consists of the following existing intersections:

- Buffaloe Road and Lucas Road
- Buffaloe Road and Quiet Oaks Drive
- Buffaloe Road and Bobbitt Drive
- Buffaloe Road and Horton Road
- Horton Road and Horton Mill Drive
- Horton Road and Old Knight Road
- Horton Road and Lucas Road

Existing peak hour traffic volumes were determined based on traffic counts conducted at the study intersection listed above, in October of 2024 during a typical weekday AM (7:00 AM – 9:00 AM) and PM (4:00 PM – 6:00 PM) peak periods. Traffic volumes were balanced between study intersections, where appropriate.



#### 3. Future Traffic Conditions

Through coordination with the Town, it was determined that an annual growth rate of 3% would be used to generate 2030 (build-out+1) projected weekday AM and PM peak hour traffic volumes. Per the Town's UDO, a 3% growth rate was applied to the existing traffic counts to project to the year 2030. For the +10 future analysis required by the Town UDO, traffic was projected beyond 2030 using a 1% growth rate. The following adjacent developments were identified to be included as an approved adjacent development in this study:

- Haywood Glen
- Weldon Village
- Brio Development

Based on coordination with the Town, no roadway improvement projects are planned within the study area.

#### 4. Site Trip Generation

Average weekday daily, AM peak hour, and PM peak hour trips for the proposed development were estimated using methodology contained within the ITE Trip Generation Manual, 11.1<sup>th</sup> Edition. Table E-1 provides a summary of the trip generation potential for the site.

Table E-1: Site Trip Generation	ation
---------------------------------	-------

Land Use (ITE Code)	Intensity	Daily Traffic	Weel AM Pea Trips	k Hour	Wee PM Pea Trips	k Hour
		(vpd)	Enter	Exit	Enter	Exit
Single Family Lots (210)	170 DU	1,644	30	91	103	61
Townhomes (215)	75 DU	522	8	25	24	17
Total Trips		2,166	38	116	127	78

#### 5. Capacity Analysis Summary

The analysis considered weekday AM and PM peak hour traffic for 2024 existing, 2030 nobuild, 2030 build, and 2039 future conditions. Refer to Section 7 of the TIA for the capacity analysis summary performed at each study intersection.



#### 6. Recommendations

Based on the findings of this study, specific geometric and traffic control improvements have been identified at study intersections. The improvements are summarized below and are illustrated in Figure E-1.

#### Improvements by Weldon Village

Horton Road and Old Knight Road

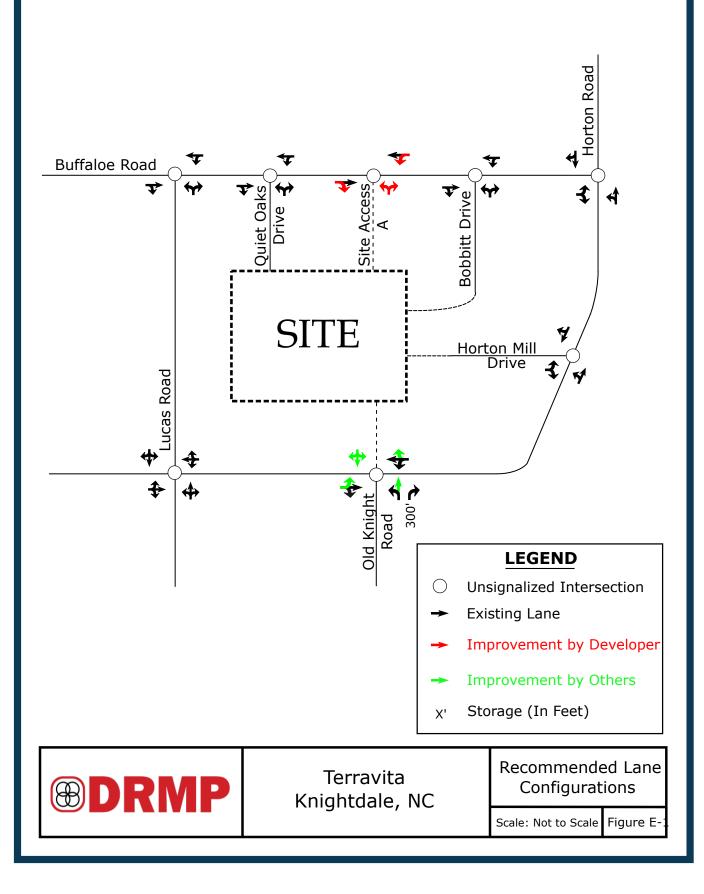
- Construct southbound approach (of Old Knight Road) with one ingress lane and one egress lane.
- Provide stop control for southbound approach.
- Construct eastbound left turn lane (on Horton Road) with 100' of storage plus appropriate deceleration and taper.

#### **Recommended Modifications by Developer**

#### Buffaloe Road and Site Access

• Construct northbound approach (of the proposed site access) with one ingress lane and one egress lane. Provide stop-control for the northbound approach.





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#### TRAFFIC IMPACT ANALYSIS

#### Terravita Knightdale, North Carolina

### **1. INTRODUCTION**

The contents of this report present the findings of the Traffic Impact Analysis (TIA) conducted for the proposed Terravita residential development to be located south of Buffaloe Road between Quiet Oaks Drive and Bobbitt Drive in Knightdale, North Carolina. The purpose of this study is to determine the potential impacts to the surrounding transportation system created by traffic generated by the proposed development, as well as recommend improvements to mitigate the impacts.

The proposed development, anticipated to be completed in 2029, is assumed to consist of the following uses:

- 170 single-family homes
- 75 townhomes

Per the Town of Knightdale's Unified Development Ordinance (UDO), the study analyzes traffic conditions during the weekday AM and PM peak hours for the following scenarios:

- 2024 Existing Traffic Conditions
- 2030 (build year+1) No-Build Traffic Conditions
- 2030 (build year+1) Build Traffic Conditions
- 2039 (build year+10) Future Traffic Conditions

#### 1.1. Site Location and Study Area

Refer to Figure 1 for the site location map.

The study area for the TIA was determined through coordination with the Town of Knightdale (Town) and consists of the following existing intersections:

- Buffaloe Road and Lucas Road
- Buffaloe Road and Quiet Oaks Drive
- Buffaloe Road and Bobbitt Drive
- Buffaloe Road and Horton Road

- Horton Road and Horton Mill Drive
- Horton Road and Old Knight Road
- Horton Road and Lucas Road

#### **1.2. Proposed Land Use and Site Access**

The proposed development is assumed to consist of the following uses:

- 170 single-family homes
- 75 townhomes

Access is proposed via one (1) new full movement driveway along Buffaloe Road and internal connections to Quiet Oaks Road, Bobbitt Drive, Proc Ridge Lane, and the Old Knight Road extension (a part of the Weldon Village adjacent development). Refer to Figure 2 for a copy of the preliminary site plan.

### 1.3. Adjacent Land Uses

The proposed development is located in an area consisting primarily of residential development.

## 1.4. Existing Roadways

Existing lane configurations (number of traffic lanes on each intersection approach), speed limits, storage capacities, and other intersection and roadway information within the study area are shown in Figure 3. Table 1 provides a summary of this information, as well.

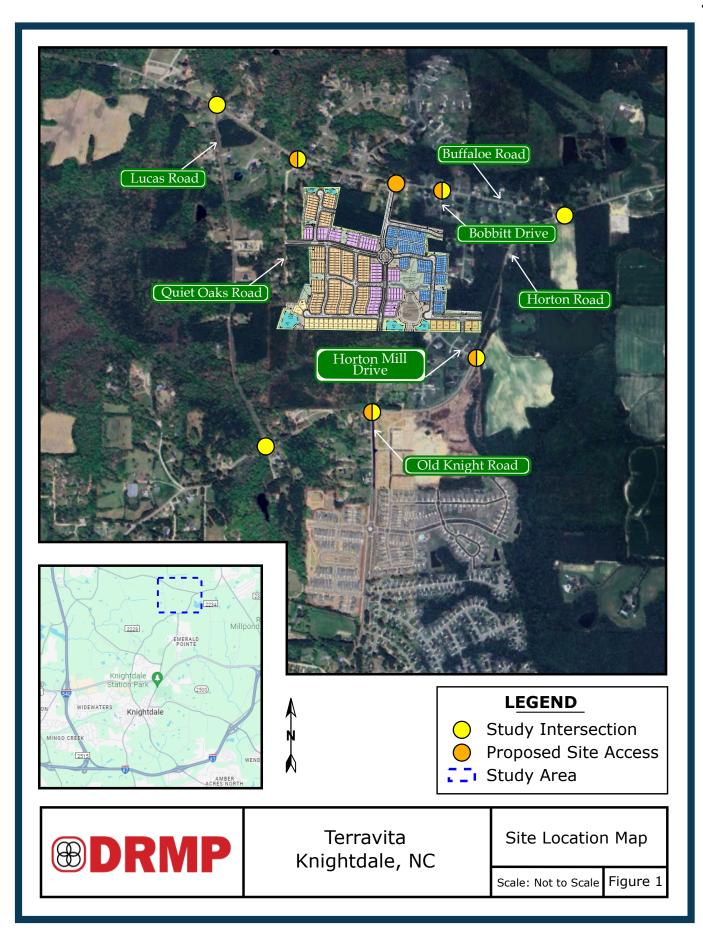


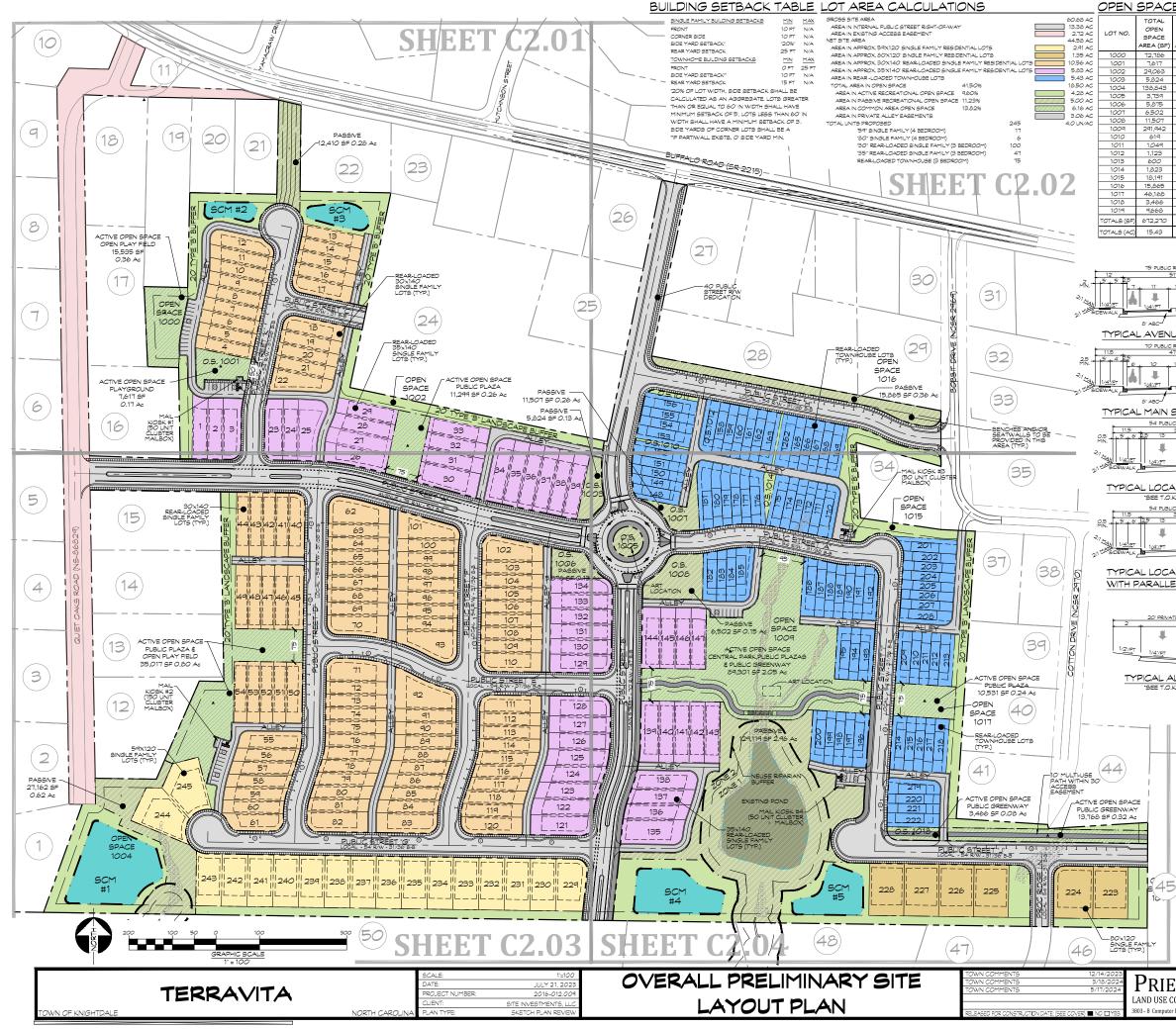
Road Name	Route Number	Typical Cross Section		
Buffaloe Road	SR 2215	2-lane undivided	45 mph	3,900
Lucas Road	SR 2260	2-lane undivided	45 mph	1,200
Bobbitt Drive	N/A	2-lane undivided	Not Posted (25 mph assumed)	*
Horton Road	SR 2231	2-lane undivided	45 mph	1,900
Horton Mill Drive	N/A	2-lane undivided	Not Posted (25 mph assumed)	*
Old Knight Road	SR 2049	2-lane undivided	45 mph	*

## Table 1: Existing Roadway Inventory

\*ADT based on the traffic counts from 2023 and assuming the weekday PM peak hour volume is 10% of the average daily traffic.







N.         OPEN         SPACE         SPA	4C	E ARE	:A TAE	BLE	LO	ΤA	RE/	<b>Α</b> Τ/	٩BL	E						
ct         space         sp	AL	ACTIVE	PASSIVE	COMMON	LOT #	(AC)	(SF)	LOT #	(AC)	(SF)	LOT #	(AC)	(SF)	LOT #	(AC)	(SF)
CE         SPACE         SP			OPEN								140	_			_	8.032
1         1									-			-			-	
10         10         0         10.00         4.16         0         0.00         4.16         0.00         4.16         0.00         4.16         0.00         4.160         0.00         8.400         0.00         8.400         0.00         8.400         0.00         8.400         0.00         8.400         0.00         8.400         0.00         8.400         0.00         8.400         0.00         8.400         0.00         8.400         0.00         8.400         0.00         8.400         0.00         8.400         0.00         0.400         0.00         0.400         0.00         0.400         0.00 <th0.00< th=""> <th0.00< th=""></th0.00<></th0.00<>											_	-			-	7,080
83       11.248       0       17.764       0       0.0 <th0< td=""><td></td><td></td><td></td><td>· · · ·</td><td>15</td><td>0.10</td><td></td><td>80</td><td>0.10</td><td></td><td></td><td>0.11</td><td></td><td></td><td>-</td><td>7,080</td></th0<>				· · · ·	15	0.10		80	0.10			0.11			-	7,080
All       O       SA24       O       SA24       O       SA40       SA40<					16	0.10	4,198	81	0.10	4,184	143	0.11	4,900	232	0.16	7,080
Na       Na <th< td=""><td></td><td></td><td>-</td><td></td><td>17</td><td>0.12</td><td>5,043</td><td>82</td><td>0.15</td><td>6,446</td><td>144</td><td>0.13</td><td>5,880</td><td>233</td><td>0.16</td><td>7,080</td></th<>			-		17	0.12	5,043	82	0.15	6,446	144	0.13	5,880	233	0.16	7,080
at       0       3.738       0         10       0.5787       0       5.778       0       1.40       1.40       1.40       1.40       2.30       0.10         12       0       0.507       0       1.1207       0       1.207       0       1.1207       0       1.1207       0       1.1207       0       1.1207       0       1.1207       0       1.1207       0       1.1207       0       1.1207       0       1.1207       0       1.1207       0       1.1207       0       1.1207       0       1.1207       0       1.1207       0       1.1207       0       1.1207 </td <td></td> <td></td> <td></td> <td></td> <td>18</td> <td>0.12</td> <td>5.046</td> <td>83</td> <td>0.14</td> <td>6.306</td> <td>145</td> <td>0.11</td> <td>4,900</td> <td>234</td> <td>0.16</td> <td>7,080</td>					18	0.12	5.046	83	0.14	6.306	145	0.11	4,900	234	0.16	7,080
15       0       5000       00       11500       00       11500       00       11500       00       11500       00       11500       00       11500       00       11500       00       11500       00       11500       00       11500       00       11500       00       11500       00       11500       00       11500       00       11500       00       11500       00       11500       00       11500       11600       11500       11600       11600       11600       11600       11600       11600       11600 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>-</td><td></td><td>_</td><td>-</td><td></td><td></td><td>-</td><td>7,080</td></t<>									-		_	-			-	7,080
C         O         TOP         TOP        TOP         TOP         TOP						-										-
Had						-			-						-	7,080
4       0       0       0       0       0       1.44       0       0.0       4.44       0       0       2.45       0.0       4.44       0       0       0.0       1.44       10       0.0       1.44       10       0.0       1.44       10       0.0       1.45       10       0.0       1.44       10       0.0       1.44       10       0.0       1.44       10       0.0       1.44       10       0.0       1.44       10       0.0       1.44       10       0.0       1.44       10       0.0       1.44       10       0.0       1.44       10       0.0       1.44       10       0.0       1.44       10       0.0       1.44       10       0.0       1.44       10       0.0       1.44       10       0.0       1.44       10       0.0       1.44       0.0       1.44       0.0       1.44       0.0       1.40       0.0       1.40       0.0       1.40       0.0       1.40       0.0       1.40       0.0       1.40       0.0       1.40       0.0       1.40       0.0       1.40       0.0       1.40       0.0       1.40       0.0       1.40       1.0       1.40       0.0					21	0.10	4,200	86	0.10	4,149	149	0.06	2,540	237	0.16	7,080
44       0       0       1.044       22       0.05       9.81       6.0       0.46       101       120       0.45       220       0.15       200       0.46       100       120       0.47       200       124       0.46       120       0.46       120       0.47       120       0.47       120       0.47       120       0.47       120       0.47       120       0.47       120       0.47       120       0.40       120       0.47       120       0.40       120       0.40       120       0.40       120       0.40       120       0.40       200       120       0.40       200       110       100       0.40       100 <td< td=""><td></td><td></td><td></td><td></td><td>22</td><td>0.13</td><td>5,627</td><td>87</td><td>0.10</td><td>4,149</td><td>150</td><td>0.06</td><td>2,645</td><td>238</td><td>0.16</td><td>7,080</td></td<>					22	0.13	5,627	87	0.10	4,149	150	0.06	2,645	238	0.16	7,080
B       O       O       1128       24       011       4×00       1×0       1×00 <td></td> <td></td> <td></td> <td></td> <td>23</td> <td><i>O</i>.13</td> <td>5,677</td> <td>88</td> <td>0.10</td> <td>4,168</td> <td>151</td> <td>0.06</td> <td>2,709</td> <td>239</td> <td>0.16</td> <td>7,080</td>					23	<i>O</i> .13	5,677	88	0.10	4,168	151	0.06	2,709	239	0.16	7,080
0       0					24	0.11	4,900	89	0 10	4 198	152	0.09	3,971	240	0.16	7,080
33       0       0       19,235         34       0       113,65       0       123,65       0       123,65       0       123,65       0       123,65       0       123,65       0       133,65       0       133,65       0       133,65       0       133,65       0       133,65       0       133,65       0       133,65       0       143,00       450       133,05       134,00       135,05       144,00       450,0       135,05       144,00       450,0       135,05       0       244       024,0       124,02       144,00       450,0       135,05       144,00       135,05       144,00       450,0       140,05       150,05       144,00       150,05       144,00       150,05       144,00       150,05       144,00       150,05       144,00       150,05       144,00       150,05       144,00       150,05       144,00       150,05       144,00       150,05       144,00       150,05       144,00       150,05       144,00       150,05       140,05       144,00       150,05       144,00       150,05       140,05       140,05       140,05       140,05       140,05       140,05       140,05       140,05       140,05       140,05       140,05 <td>0</td> <td>0</td> <td>0</td> <td>600</td> <td>28</td> <td>0.11</td> <td>5.001</td> <td></td> <td></td> <td></td> <td>15.3</td> <td>0.04</td> <td>3.950</td> <td>241</td> <td>0.16</td> <td>7,080</td>	0	0	0	600	28	0.11	5.001				15.3	0.04	3.950	241	0.16	7,080
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66       24,291       0       21,867         70       10       1400       400       40       10       420       150       150       244       120       244       120       244       120       100       420       1400       44       100       420       150       0.00       2.440       120       100       100       420       100       4200       150       0.00       2.440       100		-	-				1,0 11	91	0.10			-			-	
bell       3.466       0       0       1       1.00       430       11       1.82       100       1.00       1.24       1.42       1.00 <td></td> <td></td> <td></td> <td></td> <td>30</td> <td>0.17</td> <td>7,266</td> <td>92</td> <td>0.21</td> <td>9,170</td> <td>155</td> <td>0.06</td> <td>2,694</td> <td>243</td> <td>0.16</td> <td>7,136</td>					30	0.17	7,266	92	0.21	9,170	155	0.06	2,694	243	0.16	7,136
B0       C       Q       4660       44       0.0       4.20       155       0.06       2.440       2.40       100       1			-		31	0.11	4,900	93	0.17	7,592	156	0.09	3,876	244	0.23	10,012
270       186.425       218.003       485.845       33       0.11       4.00       46       0.10       4.20       194       0.04       2.440       1007       0.15       6         13       4.20       5.00       11.15       34       0.14       4.00       420       140       0.04       2.00       140       0.04       2.441       100       100       0.06       2.441         140       0.12       5.244       40       0.10       4.20       140       0.04       2.441       0.06       2.440       100					32	0.11	4,900	94	0.10	4,200	158	0.06	2,640	245	0.22	9,670
B3         4.28         5.00         11.15           VENC R0HT OF WAY         9         0.14         0.16         4.200         140         0.06         2.840           91         0.11         11         12         5.244         41         0.10         4.200         140         0.06         2.840           91         0.11         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110         110 <t< td=""><td></td><td></td><td></td><td></td><td>33</td><td>0 11</td><td></td><td>an.</td><td>-</td><td></td><td>159</td><td>0.06</td><td>2,640</td><td>1007</td><td>0.15</td><td>6,502</td></t<>					33	0 11		an.	-		159	0.06	2,640	1007	0.15	6,502
BID         UDUC																
UBLC RIGHT-OFWAY         II         II         III         III         IIII         IIIII         IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	+0	4.28	5.00	11.15		-						-				
UNDEC ROM-TORNAN         12         12         12         10         10         14         10         10         11         10					35	0.12	5,249	97	0.10	4,200	161					
Bit Bar         Bit Bar <t< td=""><td></td><td></td><td></td><td></td><td>36</td><td>0.12</td><td>5,249</td><td>98</td><td>0.10</td><td>4,200</td><td>162</td><td>0.06</td><td>2,640</td><td></td><td></td><td></td></t<>					36	0.12	5,249	98	0.10	4,200	162	0.06	2,640			
318.8       12       12       10       10       10       14       16       0.0       2.440       00       0.10       4.41       166       0.06       2.440         1       0       1.10       1.10       1.10       1.10       1.10       1.10       1.10       0.01       4.200       168       0.02       2.440         4       0.10       4.400       103       0.10       4.200       186       0.02       2.440         4       0.10       4.400       108       0.10       4.200       140       0.02       100       2.840       1001       0.11         10       10       4.400       106       0.10       4.200       110       0.16       4.200       110       0.16       2.840       1000       1.11         10       10       4.401       106       0.10       4.200       112       0.40       113       0.40       113       100       1.11       100       1.10       100       1.10       100       1.11       100       1.11       100       1.11       100       1.11       100       1.11       100       1.11       100       1.11       1.11       1.11       1.11	UBLIC		r		37	0.12	5,249	99	0.10	4,200	163	0.09	3,840			
10       11       11       12       11       10       1.1       10       0.15       6.471       106       0.26       2.840       DPEN         10       0.15       0.21       5.35       101       0.15       6.471       106       0.26       2.840       DPEN         11       0.10       4.400       105       0.10       4.200       116       0.04       2.840       100       1.81         12       0.10       4.401       105       0.10       4.200       110       0.04       3.841       100       1.81         14       0.10       4.401       105       0.01       4.200       110       0.04       2.840       100       0.11         14       0.10       4.401       106       0.00       4.200       111       0.06       2.840       100       0.01       4.11         15       0.10       4.401       106       0.00       4.200       114       0.06       2.840       100       0.01       2.11       0.00       2.840       100       0.01       1.11         16       0.10       4.401       100       0.40       4.200       114       0.10       2.840	5020	1 B-B		12	38	0.12	5,249	100	0.10	4,216	165	0.06	2,640			
Image: Second and the second		10' . 11'	7 25 5	5	34		5,232	-			166	0.06	2,640			
Image: Normal Section	1	c 🔺				-						-			PEN	N
4         0,10         4.400         100         0,10         4.200         100         0,20         3.844         LOT#         (AC)           VIL: 9838         25:113.03         4.400         104         0.00         4.200         110         0.04         8.821         1000         1.81           VALUE RIGHT-ORWAY         4.400         104         4.400         105         0.10         4.200         111         0.02         2.448         1000         0.11           VALUE RIGHT-ORWAY         4.401         105         0.10         4.200         113         0.02         2.448         1004         0.01         3.00         1.00         0.01         3.00         1.00         0.01         3.00         0.02         3.849         1.00         0.01         3.00         1.00         0.01         3.11         1.00         3.00         1.00         1.00         1.00         3.11         1.00         3.00         3.00         1.00         3.00         1.00         3.00         1.00         3.00         1.00         1.00         3.00         1.00         3.00         1.00         3.00         1.00         1.00         1.00         1.00         1.00         3.00         1.00	F	POINT		FT DUMAN				-	-					-		
42         0.10         4.400         104         0.10         4.200         104         0.00         3.243         Lota         (42)           ENUE STREET SECTION         43         0.10         4.400         105         0.10         4.200         110         0.00         3.243         Lota         (42)           10         10         10         10         10         10         100         111         0.00         2.840         1000         111           10         10         10         10         10         10         100         111         0.00         2.840         1000         0.10         4.200         111         0.00         2.840         1000         0.11           10         10         4.401         110         0.10         4.200         113         0.00         2.841         1000         0.13           11         10.10         4.401         110         0.14         4.01         110         0.14         100         1.15         0.00         2.841         1000         0.13         100         1.15         1.15         100         1.15         1.10         1.10         1.10         1.10         1.10         1.10		4 H		DEWALK KAL	41	0.10		103	0.10	4,200	168	-		_		-
44       0.10       4.401       105       0.10       4.200       110       0.40       2.44       100       0.11         47       8.30       11.5       1.5       1.5       0.10       4.200       111       0.40       2.440       100       0.10       4.200       111       0.40       2.440       100       0.10       4.200       111       0.40       2.440       100       0.10       4.200       111       0.40       2.440       100       0.10       4.200       111       0.40       2.440       100       0.10       4.200       111       0.40       2.440       100       0.10       4.200       113       0.40       2.441       100       4.401       100       4.401       100       4.401       100       4.401       100       4.401       100       4.401       110       0.14       4.401       100       4.401       100       4.401       100       4.401       101       4.401       100       4.401       101       4.401       101       4.401       101       4.401       101       4.401       101       4.401       101       4.401       101       4.401       101       4.401       101       4.401       10	1		1.5B	9	42	0.10	4,400	104	0.10	4,200	169	0.09		LOT #	(AC)	(SF)
44       0.10       4.401       100       0.10       4.200       111       0.00       2.646       1001       0.11         45       0.12       5.423       107       0.10       4.200       112       0.06       2.646       1004       3.18       1         46       0.10       4.401       106       0.10       4.200       112       0.06       2.640       1004       3.18       1         47       0.10       4.401       104       0.10       4.200       117       0.06       2.640       1006       0.13         48       0.12       5.423       107       0.10       4.200       117       0.06       2.640       1006       0.01         49       0.10       4.401       110       0.10       4.200       117       0.06       2.624       1006       0.10         101       102       0.10       4.200       111       0.10       4.200       111       0.06       2.804       1006       0.10         101       102       0.10       4.200       111       0.10       4.201       111       0.10       4.201       110       0.10       4.201       100       0.10       <	- /ENII	-2½"11	19.0B		43	0.10	4,401	105	0.10	4,200	170	0.09	3,927	1000	1.67	72,786
UBUC RIGHTOR WAY         113         113         113         113         113         113         113         113         113         113         113         113         113         114         0.00         2.840         1000         0.13           10         10         10         10         10         10         10.0         10.0         10.0         2.840         1000         0.13           11         10         10         10.0         10.0         10.0         10.0         10.0         10.0         2.800         1000         0.13         1000         0.13           11         10.0         11.0         0.10         4.200         113         0.00         4.200         117         0.06         2.801         1000         0.10         1000         0.00         10.0         0.00         10.0         0.00         0.00         10.0         0.00					44	0.10	4,401	106			171	0.06	2,648	1001	0 17	7.617
10       10 <td< td=""><td></td><td></td><td></td><td>15</td><td></td><td>-</td><td></td><td></td><td>-</td><td></td><td></td><td></td><td></td><td></td><td></td><td>5,824</td></td<>				15		-			-							5,824
41         0.10         4.40         100         0.10         4.20         114         0.00         2.62         10.05         0.09         10.05           10         0.10         4.40         110         0.10         4.20         114         0.00         2.62         10.05         0.09         10.05         0.09         10.05         0.09         10.05         0.09         10.05         0.09         10.05         0.09         10.05         0.09         10.05         0.09         10.05         0.09         0.09         10.05         0.09         0.05         0.09         0.01 <t< td=""><td>4</td><td></td><td>2,5 4</td><td></td><td></td><td></td><td></td><td></td><td>-</td><td></td><td></td><td>-</td><td></td><td></td><td></td><td></td></t<>	4		2,5 4						-			-				
Investigation         Investig	+	10 10	-+6-													138,84
Investigation         Investig	F	GRADE		The state	47	0.10	4,401	109	0.10	4,200		-		1005	0.09	3,739
Investigation         Investig	T	POINT 1/41/			48	0.10	4,401	110	0.14	6,026	175	0.09	3,806	1006	0.13	5,875
Solution		L-1% 99	1.58		49	0.10	4,401	111	0.13	5,466	176	0.09	3,956	1007	0.15	6,502
NN STREET SECTION       112       0.12       0.10       120       0.10       110       0.01       110       0.01       2.00       0.01       100       0.01 <td></td> <td><u></u>2½°+1</td> <td>19.OB</td> <td></td> <td>50</td> <td>-</td> <td>5 180</td> <td></td> <td>0 10</td> <td>4,200</td> <td>177</td> <td>0.06</td> <td>2,804</td> <td></td> <td></td> <td>11,501</td>		<u></u> 2½°+1	19.OB		50	-	5 180		0 10	4,200	177	0.06	2,804			11,501
PLOLE CRIGHT-OF-WAY				N					-			-				291,94
19       19       24       6       5       0.10       4.200       115       0.10       4.141       101       0.01       0.21       0.21       101       0.02       0.21       101       0.02       0.21       101       0.02       0.21       101       0.02       0.21       101       0.02       0.22       0.02       0.22       0.02       0.22       0.02       0.22       0.02       0.22       0.02       0.22       0.02       0.22       0.02       0.22       0.02       0.22       0.02       0.22       0.02       0.22       0.02       0.22       0.02       0.22       0.02       0.22       101       0.02       0.22       0.04       0.22       0.04       0.22       0.04       0.22       0.04       0.22       0.04       0.23       101       0.02       0.26       0.26       0.10       0.26       0.10       0.26       0.10       0.26       0.10       0.26       0.10       0.21       0.10       0.10       1.11       1.06       0.26       0.10       0.26       0.10       1.01       0.06       0.10       1.01       0.06       1.01       0.06       1.01       0.06       0.11       1.01       0.06	PUBL								-	-						-
PARL         59         0.10         4.200         115         0.10         4.16         100         0.00         9.21         101         0.02           VIT         V	13'		2,5 6 5	0.5	52	0.10		114	0.10	4,197		-		1010	0.01	619
Image: Second Market	10			Min.	53	0.10	4,200	115	0.10	4,165	180	0.07	3,221	1011	0.02	1,049
1         0         1         0         1         0         1         0         1         0         1         0         1         0         1         0         1         0         1         0	₩.			×4.	54	0.10	4,200	116	0.10	4,149	181	0.11	4,993	1012	0.09	3,754
SDEWALK         56         0.10         4.390         116         0.10         4.155         183         0.06         2.815           OCAL STREET SECTION         57         0.10         4.393         114         0.10         4.162         184         0.06         2.866         1016         0.36           TOCK STD. DETAIL 3.02         PUBLIC RIGHT-OF-WAY         55         0.10         4.371         120         0.13         5.466         105         0.01         2.851         1016         0.06           36' 9.3         11         7.26 6.5         0.5         0.5         0.10         4.211         122         0.12         5.405         186         0.06         2.170           10         0.01         4.211         124         0.15         5.405         186         0.06         2.170           11         124         0.12         5.405         186         0.06         2.170           12         0.11         4.450         124         0.12         5.428         180         0.06         2.170           12         0.11         4.450         124         0.12         5.428         180         0.06         2.170           12         0	<u>7</u> FT	POINT 1/	4"/ET 1/4/F		55	0.13	5,511	117	0.10	4,149	182	0.08	3,552	1014	0.04	1,823
Product         Product <t< td=""><td>-</td><td>T.</td><td>SIDEN</td><td>VALK</td><td></td><td></td><td></td><td></td><td></td><td>4 155</td><td>183</td><td>0.06</td><td>2,581</td><td></td><td>-</td><td>19,419</td></t<>	-	T.	SIDEN	VALK						4 155	183	0.06	2,581		-	19,419
Since         Since <th< td=""><td></td><td>—8° A</td><td>BC</td><td></td><td></td><td>-</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th<>		—8° A	BC			-										
10.1       0.01       10.1       10.1       0.01       10.1       10.1       0.01       10.1       0.01       10.1       0.01       10.1       0.00       10.1       0.00       10.1       0.00       10.1       0.00       10.1       0.00       10.1       0.00       10.1       0.00       10.1       0.00       10.1       0.00       10.1       0.00       10.1       0.00       10.1       0.00       10.1       0.00       10.1       0.00       10.1       0.00       10.1       0.00       10.1       0.00       10.1       0.00       10.1       0.00       10.1       10.1       0.00       10.1       10.1       0.00       10.1       10.1       10.1       10.1       10.1       10.1       10.1       10.1       10.1       10.1       10.1       10.1       10.1       10.1       10.1       10.1       10.1       10.1       10.1				<u>FION</u>								-				15,865
10       0.10       11       12       0.10       0.10       0.10       0.00       0.00         10       11       1.2       0.10       1.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.20       0.00 <td>т.о.</td> <td>K. STD. DET,</td> <td>AIL 3.02</td> <td></td> <td>58</td> <td>0.10</td> <td>4,371</td> <td>120</td> <td>0.13</td> <td>5,466</td> <td>185</td> <td>-</td> <td></td> <td>1017</td> <td>1.06</td> <td>46,168</td>	т.о.	K. STD. DET,	AIL 3.02		58	0.10	4,371	120	0.13	5,466	185	-		1017	1.06	46,168
13         11         1.2         2.4         9.5           28         24.2         9.5         9.5         9.6         0.10         4.21         112         0.12         5.405         184         0.06         2.110         101         0.22           24         9.43C         9.42C         9.10         124         0.12         5.405         184         0.06         2.113           22/         945.4         502WALK         64         0.10         4.200         1124         0.12         5.853         181         0.06         2.113           64         0.10         4.200         112         0.12         5.853         191         0.06         2.113           64         0.10         4.200         112         0.12         5.853         191         0.06         2.113           64         0.10         4.200         112         0.12         5.318         192         0.04         3.840           0         0.10         4.200         112         0.14         6.800         2.10         0.66         2.840           66         0.10         4.200         113         0.11         4.800         212         0.06			AY		59	0.10	4,279	121	0.15	6,333	187	0.07	2,837	1018	0.08	3,466
PARKING         PARK           4         0.11         4.450         123         0.12         5.405         194         0.06         2.120           VET         VEX         124.012         5.405         194         0.06         2.113           202 SH5A         SDEWALK         4200         125         0.12         5.405         194         0.06         2.113           CAL STREET SECTION         44         0.10         4.200         126         0.12         5.320         210         0.06         2.840           66         0.10         4.200         126         0.12         5.310         120         0.64         2.840           66         0.10         4.200         126         0.12         5.310         100         2.640           66         0.10         4.200         126         0.14         6.00         2.840           61         0.10         4.200         130         0.11         4.400         220         0.66         2.840           61         0.10         4.200         130         0.11         4.400         220         0.66         2.840           70         0.15         6.48         132		36' B-B	6		60	0.10	4,211	12.2	0.12	5,430	188	0.06	2,770	1019	0.22	9,668
Image: Construction of the state o	10		PARKING	- Miñ.	61	0.11	4,950	123	0.12	5,405	189	0.06	2,720	<u> </u>		
Image: set of the set	+	¢ T		~~~~·				-	-		190	-	2 713			
PRIVATE RIGHT-OF-WAY         V2/15T	<u>:/</u> FT	POINT 1/2	47/ET 1/4	FRAN							_	-				
PRIVATE RIGHT-OF-WAY         2         2         0.10         4.200         112         0.11         5.310         142         0.04         3.512           VEXTER RIGHT-OF-WAY         65         0.10         4.200         112         0.11         5.330         210         0.06         2.840           VEXTER RIGHT-OF-WAY         66         0.10         4.200         112         0.11         4.800         211         0.06         2.840           VEXTER RIGHT-OF-WAY         66         0.10         4.200         113         0.11         4.800         213         0.09         3.840           VEXTER RIGHT-OF-WAY         16         0.10         4.200         131         0.11         4.800         213         0.09         3.840           16         0.10         4.200         131         0.11         4.800         220         0.06         2.840           170         0.15         6.485         132         0.11         4.800         221         0.06         2.840           171         0.16         6.862         133         0.11         4.800         222         0.06         2.840           172         0.10         4.200         136         0.				DEWALK	63	-		125	-							
BRUATE RIGHT-OF-WAY         2         0         0         4.200         122         0.14         6.802         211         0.06         2.840           PRVATE RIGHT-OF-WAY         16         0.10         4.200         124         0.15         5,746         212         0.06         2.840           PRVATE RIGHT-OF-WAY         16         0.10         4.200         130         0.11         4.900         213         0.09         3.840           16         0.10         4.200         130         0.11         4.900         212         0.06         2.840           10         0.15         6.465         132         0.11         4.900         212         0.06         2.840           11         0.16         6.862         133         0.11         4.900         222         0.06         2.840           11         0.16         6.862         133         0.11         4.900         222         0.02         3.840           12         0.10         4.200         134         0.11         4.900         222         0.22         4.600           12         0.10         4.200         135         0.16         7.884         224         0.25		1 21/2" 8" A			64	0.10	4,200	126	0.12	5,318	192	0.09	3,812			
PRVATE RIGHT-OF-WAY         61         0.10         4.200         1124         0.15         5.746         212         0.06         2.840           68         0.10         4.200         1130         0.11         4.400         213         0.04         3.840           64         0.10         4.200         1131         0.11         4.400         213         0.04         3.840           16         0.01         4.200         1131         0.11         4.400         220         0.06         2.840           10         0.18         6.862         1132         0.11         4.400         222         0.06         2.840           11         0.16         6.862         133         0.11         4.400         222         0.06         2.840           12         0.10         4.200         134         0.11         4.800         222         0.02         8.840           12         0.10         4.200         135         0.11         4.704         224         0.22         10.02         113         0.12         5.904         2.24         0.25         10.124           13         0.10         4.200         135         0.12         5.904		L STRE	ET SECT	<i>FION</i>	65	0.10	4,200	127	0.12	5,320						
PRVATE RIGHT-OF-WAY         61         0.10         4.200         1124         0.15         5.746         212         0.06         2.840           68         0.10         4.200         1130         0.11         4.400         213         0.04         3.840           64         0.10         4.200         1131         0.11         4.400         213         0.04         3.840           16         0.01         4.200         1131         0.11         4.400         220         0.06         2.840           10         0.18         6.862         1132         0.11         4.400         222         0.06         2.840           11         0.16         6.862         133         0.11         4.400         222         0.06         2.840           12         0.10         4.200         134         0.11         4.800         222         0.02         8.840           12         0.10         4.200         135         0.11         4.704         224         0.22         10.02         113         0.12         5.904         2.24         0.25         10.124           13         0.10         4.200         135         0.12         5.904					66	0.10	4,200	128	0.14	6,306	211	0.06	2,640			
PRIVATE RIGHT-OF-WAY         0         0         0         10         10         10         0         0         11         4,60         215         0.04         3,840           10         0         0         10         0         11         0         11         4,800         215         0.04         3,840           10         0         0         15         0.11         4,800         220         0.06         2,843           70         0.15         6,485         132         0.11         4,400         220         0.06         2,840           71         0.16         6,862         133         0.11         4,600         222         0.04         3,840           72         0.10         4,200         134         0.11         4,700         224         0.06         2,440           72         0.10         4,200         135         0.11         1,784         224         0.25         10,724           74         0.10         4,200         136         0.12         5,743         225         0.22         4,800           75         0.10         4,200         136         0.12         5,745         227 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>																
PRIVATE RIGHT-OF-WAY         64         0.10         4.200         191         0.11         4.800         220         0.06         2.643           16         0         0         15         6.485         192         0.11         4.800         221         0.06         2.643           10         0         15         6.485         192         0.11         4.800         221         0.06         2.640           11         0.16         6.862         193         0.11         4.800         222         0.06         3.840           12         0.10         4.200         194         0.11         4.784         223         0.22         4.800           12         0.10         4.200         195         0.11         4.784         224         0.22         4.800           13         0.10         4.200         196         0.12         5.794         225         0.22         4.800           14         0.10         4.200         197         0.12         5.414         226         0.22         4.800           15         0.10         4.304         198         0.14         5.908         221         0.22         4.800      1																
16         2         0.1         4.80         21         0.0         2.6.40           10         0.16         6.485         132         0.11         4.802         221         0.06         2.6.40           11         0.16         6.485         133         0.11         4.802         222         0.06         2.6.40           11         0.16         6.862         133         0.11         4.900         222         0.04         3.840           12         0.10         4.200         134         0.11         4.184         223         0.22         4.600           13         0.10         4.200         135         0.15         7.84         224         0.25         10.724           14         0.10         4.200         135         0.12         5.043         225         0.22         4.600           15         0.10         4.200         136         0.12         5.043         225         0.22         4.600           15         0.10         4.200         136         0.12         5.141         226         0.22         4.600           16         0.10         4.344         135         0.14         5.908																
VPT         COUNT         V/4/167         V/2/171           V21         0.10         6.862         132         0.11         4.400         221         0.06         2.840           11         0.16         6.862         133         0.11         4.900         222         0.02         3.840           12         0.10         1.20         114         0.11         4.764         223         0.22         4.800           12         0.10         1.20         1154         0.11         4.764         224         0.25         10.12           26: e85.a         130         0.10         136         0.12         5.042         2.24         0.25         10.12           13         0.10         4.200         135         0.11         7.894         2.24         0.25         10.12           14         0.10         4.200         136         1.12         5.042         2.25         0.22         4.800           15         0.10         4.200         137         0.12         5.141         2.26         0.22         4.800           16         0.10         4.304         139         0.14         5.908         2.21         0.22 <t< td=""><td>PRIVA</td><td>TE RIGHT-OF-W 16'</td><td>AY ?</td><td>-1</td><td>69</td><td>0.10</td><td></td><td>131</td><td>0.11</td><td></td><td>-</td><td></td><td></td><td></td><td></td><td></td></t<>	PRIVA	TE RIGHT-OF-W 16'	AY ?	-1	69	0.10		131	0.11		-					
CONT         V2/FT         V2/FT         V2/FT           PONT         V4/VET         V2/FT         12         0.10         4.200         113         0.11         4.784         223         0.22         4.600           VEX         V2/FT         V2/FT         13         0.10         4.200         113         0.10         4.200         135         0.10         4.204         0.25         10.712           VEX         SECTION         T4         0.10         4.200         135         0.10         5.033         225         0.22         4.600           T4         0.10         4.200         137         0.12         5.141         226         0.22         4.600           T5         0.10         4.200         137         0.12         5.141         226         0.22         4.600           T6         0.10         4.394         139         0.14         5.905         221         0.22         4.600	11			-1	70	0.15	6,485	132	0.11	4,900	221	0.06	2,640			
Construction         Construction<	₩.	ę 🎵			71	0.16	6,862	133	0.11	4,900	222	0.09	3,840			
14         0.10         4.200         136         0.12         5.093         2.25         0.22         4.600           T.O.K. STD. DETAIL 3.01         75         0.10         4.200         137         0.12         5.141         226         0.22         4.600           T6         0.10         4.200         137         0.12         5.141         226         0.22         4.600	-/	POINT .	(41/ET 1/21/FT	r I	72		4,200			4,789	223	0.22	9,600			
14         0.10         4.200         136         0.12         5.093         2.25         0.22         4.600           T.O.K. STD. DETAIL 3.01         75         0.10         4.200         137         0.12         5.141         226         0.22         4.600           T6         0.10         4.200         137         0.12         5.141         226         0.22         4.600	<u>/F</u> T	- V	4/11 2	_		-				-						
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76 0.10 4.199 138 0.14 5.908 227 0.22 9.600	T.O.	K. STD. DET.	AIL 3.01		75	0.10	4,200	137	0.12	5,141	226	0.22	9,600			
					76	0.10	4,199	138	0.14	5,908	227	0.22	9,600			
					77	0.10	4,175	139	0.14	5,936	228	0.22	9,600			
					<u> </u>											

#### GENERAL NOTES:

- 1. THE CONCEPTUAL PLAN WAS PREPARED BY CHARLES R. WALKER, III, PLA AND ENTITLEMENT PRESERVATION GROUP.
- 2. THIS PLAN IS CONCEPTUAL IN NATURE AND SUBJECT TO CHANGE AS DESIGN PROGRESSES
- 3. BOUNDARY INFORMATION IS TAKEN FROM A SURVEY BY THIS OFFICE
- SITE TOPOGRAPHIC INFORMATION IS TAKEN FROM A COMBINATION OF DATA FROM A SURVEY PERFORMED BY THIS OFFICE AND WAKE COUNTY GIS INFORMATION.
- PLANEMETRIC AND TOPOGRAPHIC INFORMATION FOR AREAG OUTSIDE OF THIS SITE ARE TAKEN FRO WAKE COUNTY GIS INFORMATION.
- ALL MATERIALS AND CONSTRUCTION SHALL BE IN STRICT ACCORDANCE WITH THE TOWN O KNIGHTDALE, NODOT, AND NODEQ STANDARDS AND SPECIFICATIONS.
- 7. THERE ARE NO FEMA DESIGNATED FLOOD ZONES LOCATED ON THIS PROPERTY
- EXISTING UTILITIES SHOWN ARE APPROXIMATE. CONTRACTOR RESPONSIBLE FOR LOCATION OF ALL EXISTING ABOVE AND BELOW GROUND UTILITY FIELD LOCATION PRIOR TO ANY CONSTRUCTION.
- 9. NO NEW BUFFER IMPACTS SHALL OCCUR PRIOR TO APPROVAL FROM NCDEQ.
- 10. WETLAND AND STREAM BUFFER LOCATIONS ARE SUBJECT TO FIELD VERIFICATION.
- 11. STORMWATER CONTROL MEASURES ARE CONCEPTUAL AND ARE SUBJECT TO FUTURE SIZING CALCULATIONS AND DESIGN.

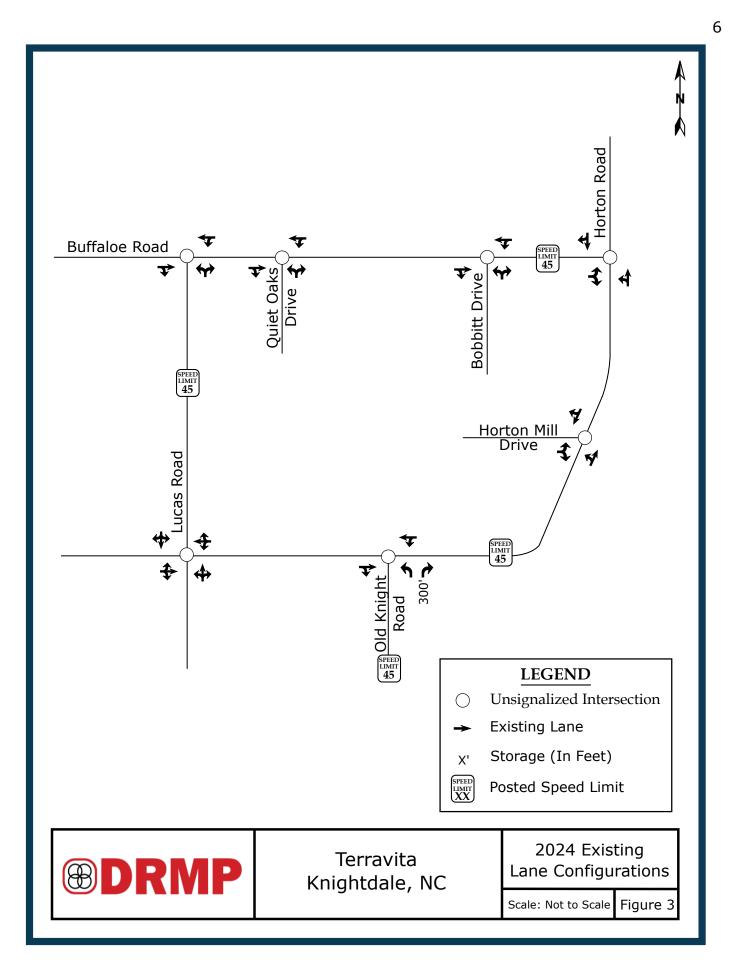


SHEET #

C2.00

#### PRIEST, CRAVEN & ASSOCIATES, INC. LAND USE CONSULTANTS PLANNERS / LANDSCAPE DESIGNERS / SURVEYORS / ENGINEERS

LAND USE CONSULTANTS PLANNERS / LANDSCAPE DESIGNERS / SURVEYORS / ENGINEERS 1803 - B Computer Drive, Suite 104 Raleigh, NC. 27609. Phone 919 / 781-0300. Fax 919 / 782-1288. Email PCA@PriestCraven.com / Firm #: C-0488



## 2. 2024 EXISTING PEAK HOUR CONDITIONS

## 2.1. 2024 Existing Peak Hour Traffic Volumes

Existing peak hour traffic volumes were determined based on traffic counts conducted at the study intersections listed below, in October of 2024 during a typical weekday AM (7:00 AM – 9:00 AM) and PM (4:00 PM – 6:00 PM) peak periods:

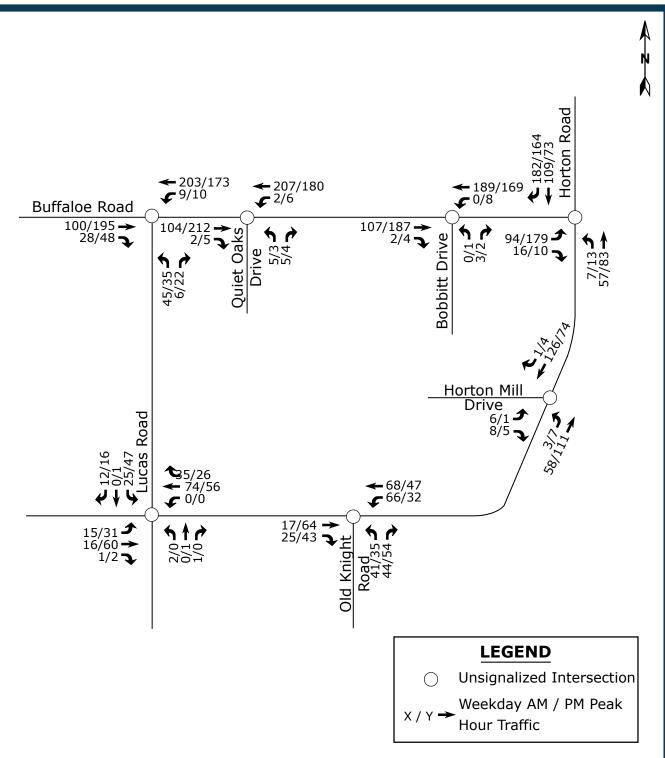
- Buffaloe Road and Lucas Road
- Buffaloe Road and Quiet Oaks Drive
- Buffaloe Road and Bobbitt Drive
- Buffaloe Road and Horton Road
- Horton Road and Horton Mill Drive
- Horton Road and Old Knight Road
- Horton Road and Lucas Road

Weekday AM and PM traffic volumes were balanced between study intersections, where appropriate. It should be noted that traffic volumes at the intersection of Buffaloe Road and Quiet Oaks Drive were not recorded. Google Earth and the Town parcel map shows that 16 single family homes are located along Quiet Oaks Drive. The Institute for Transportation Engineers (ITE) Trip Generation Manual, 11<sup>th</sup> edition, was used to generate traffic for those 16 single-family homes. Through volumes were then balanced along Buffaloe Road with the Lucas Road intersection. Refer to Figure 4 for 2024 existing weekday AM and PM peak hour traffic volumes. A copy of the count data is located in Appendix B of this report.

## 2.2. Analysis of Existing Peak Hour Traffic Conditions

The 2024 existing weekday AM and PM peak hour traffic volumes were analyzed to determine the current levels of service at the study intersections under existing roadway conditions. The results of the analysis are presented in Section 7 of this report.





Note: Based on NCDOT Congestion Management guidelines, a volume of 4 vehicles per hour (vph) was analyzed for any movement with less than 4 vph.



## 3. 2030 NO-BUILD PEAK HOUR CONDITIONS

In order to account for growth of traffic and subsequent traffic conditions at a future year, no-build traffic projections are needed. No-build traffic is the component of traffic due to the growth of the community and surrounding area that is anticipated to occur regardless of whether or not the proposed development is constructed. No-build traffic is comprised of existing traffic growth within the study area and additional traffic created as a result of adjacent approved developments.

## 3.1. Ambient Traffic Growth

Through coordination with the Town, it was determined that an annual growth rate of 3% would be used to generate 2030 projected weekday AM and PM peak hour traffic volumes. Per the Town UDO, a 1% growth rate was applied to the projected traffic for every year after 2030 in the future analysis. Refer to Figures 5a and 5b for 2030 and 2039 projected peak hour traffic, respectively.

## 3.2. Adjacent Development Traffic

Through coordination with the Town, the following adjacent developments were identified to be included as an approved adjacent development in this study:

- Haywood Glen
- Weldon Village
- Brio Development

Table 2, on the following page, provides a summary of the adjacent developments.



Development Name	Location	Build-Out Year	Land Use / Intensity	TIA Performed
Haywood Glen	Southeast quadrant of Horton Road and Old Knight Road	2025	107 single-family homes and 10,000 s.f. of commercial	N/A Trip generation letter applied to roadway network
Weldon Village	South of proposed site, internal connectivity proposed	2029	Mixed-use consisting of residential, office, and retail	October 2022 By RKA
Brio Development	South of Buffaloe Road, west of Lucas Road	2027	Mixed-use residential and retail	May 2021 By RKA

#### **Table 2: Adjacent Development Information**

The Haywood Glen development is expected to be constructed by the end of 2025. After the TIA was approved, a trip generation letter was done for the proposed site, adding on commercial square footage. The trip generation from the letter was distributed based on distributions for the proposed site and engineering judgement. Weldon Village is expected to be constructed the same year as the proposed development and are proposed to have interconnectivity. Roadway improvements at the intersection of Horton Road and Old Knight Road are considered under all future analysis conditions of the proposed site. The Brio development along Buffaloe Road, west of the proposed site, is expected to be constructed by the end of 2027. Site trips expected to utilize the study area were included in all future analysis.

It should be noted that the adjacent developments were approved, during scoping, by the Town. Adjacent development trips are shown in Figure 6. Adjacent development information can be found in Appendix C.

## **3.3. Future Roadway Improvements**

Based on coordination with the Town, it was determined there were no future roadway improvements to consider with this study.



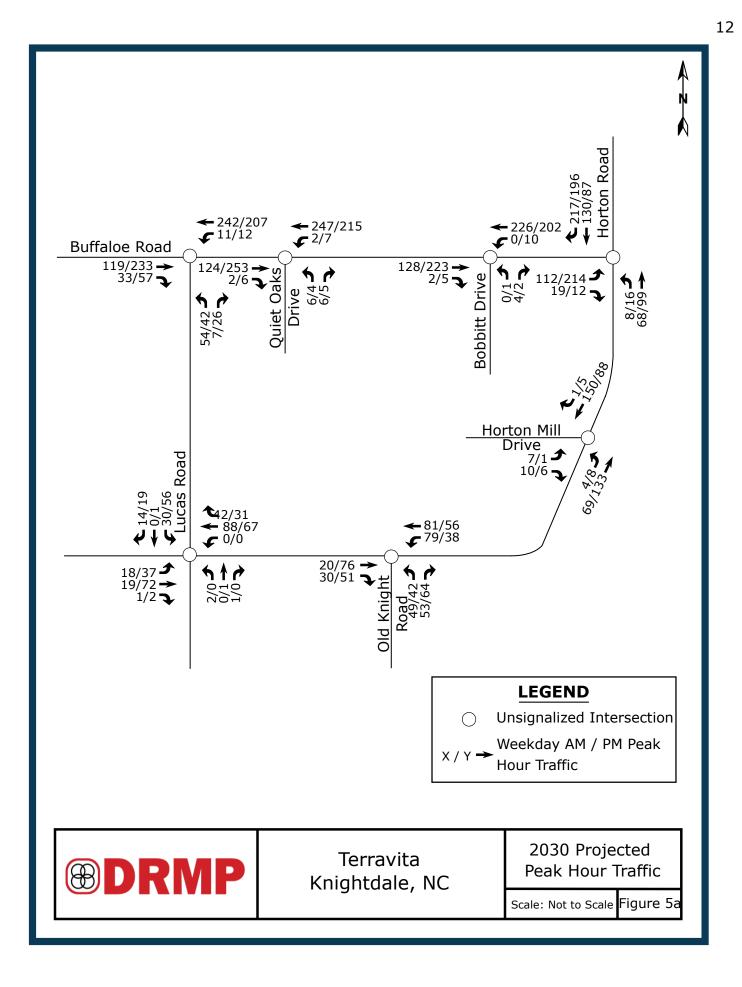
## 3.4. No-Build Peak Hour Traffic Volumes

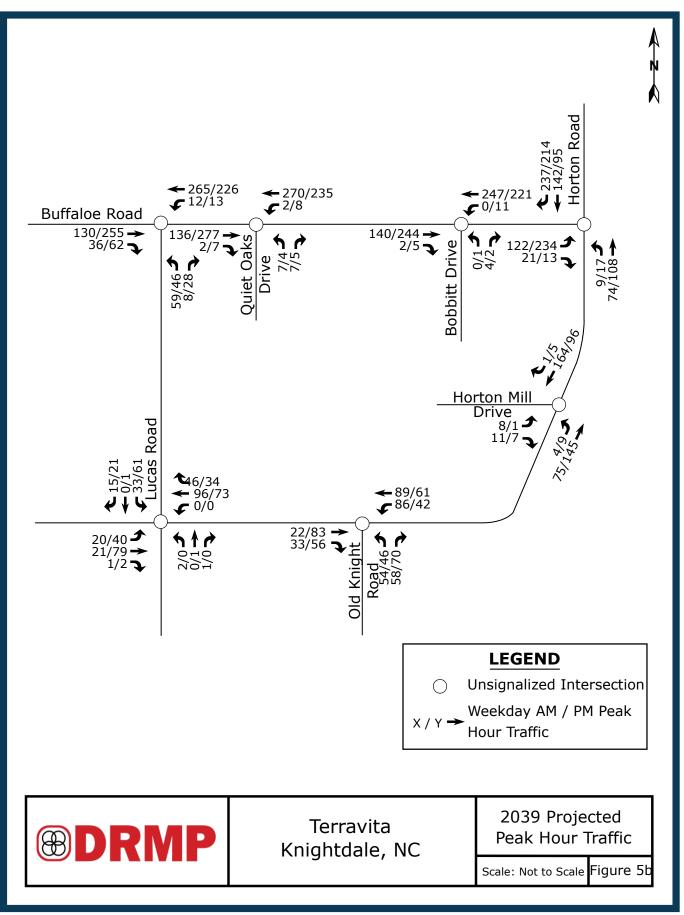
The 2030 no-build traffic volumes were determined by projecting the 2024 existing peak hour traffic to the year 2030, and adding the adjacent development trips. For the future analysis, a 1% growth rate was applied beyond the year 2030 to 2039. Refer to Figures 7a and 7b for illustrations of the 2030 and 2039 no-build peak hour traffic volumes at the study intersections.

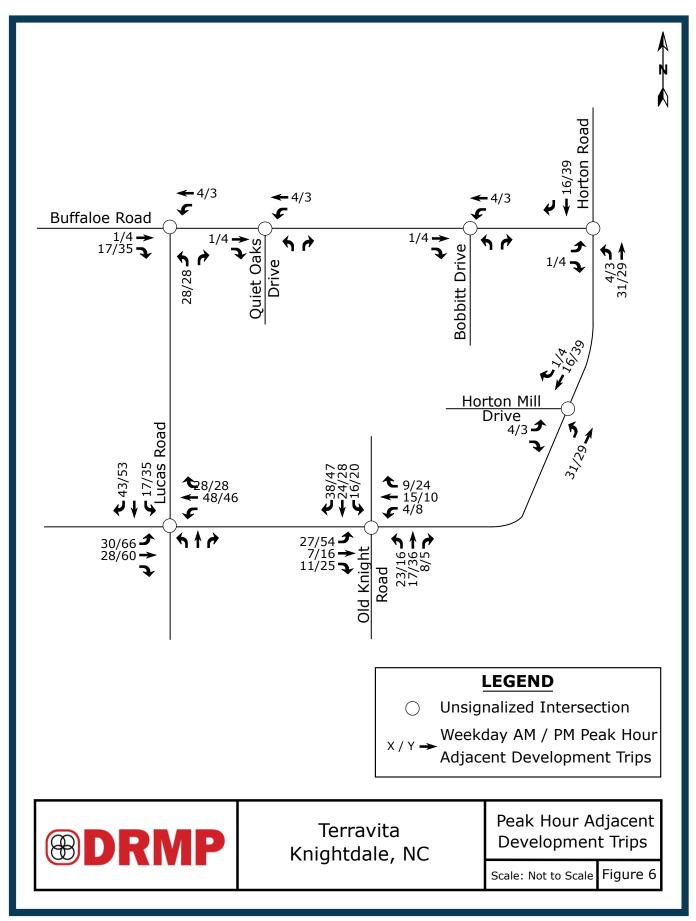
## 3.5. Analysis of No-Build Peak Hour Traffic Conditions

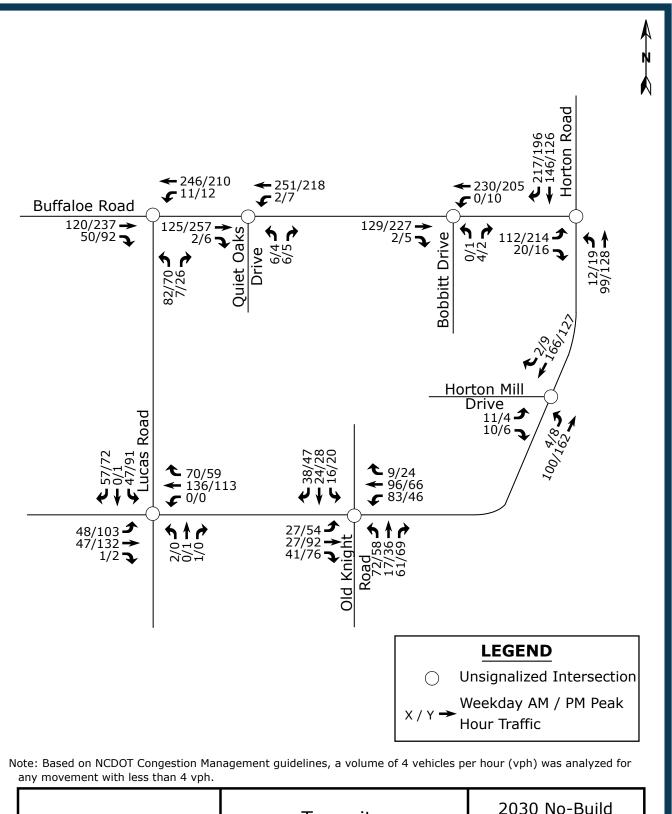
The 2030 no-build AM and PM peak hour traffic volumes at the study intersections were analyzed with future geometric roadway conditions and traffic control. The analysis results are presented in Section 7 of this report.

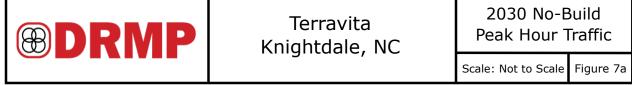


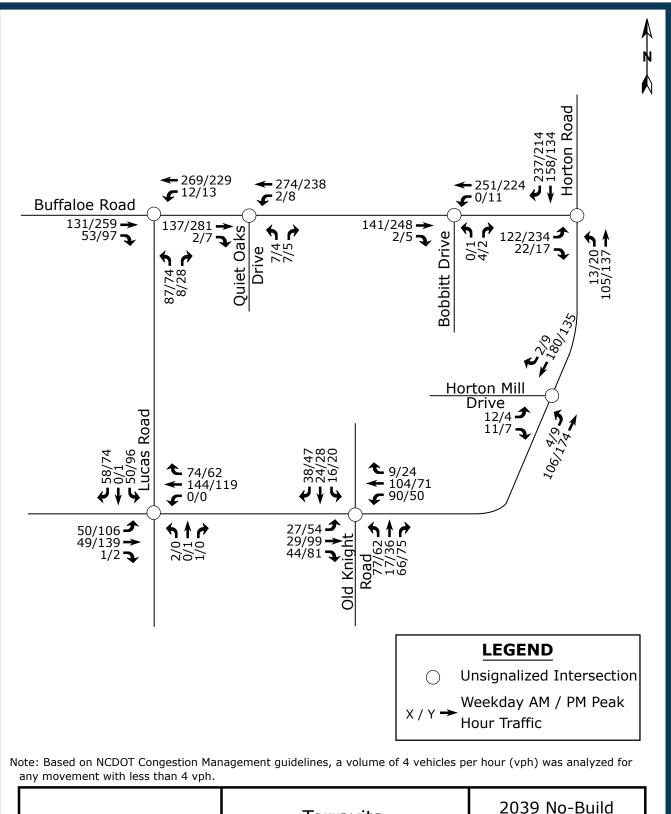














## 4. SITE TRIP GENERATION AND DISTRIBUTION

### 4.1. Trip Generation

Average weekday daily, AM peak hour, and PM peak hour trips for the proposed development were estimated using methodology contained within the ITE *Trip Generation Manual*, 11.1 Edition. Table 3 provides a summary of the trip generation potential for the site.

Land Use (ITE Code)	Intensity	Daily Traffic	Weeł AM Pea Trips (	k Hour	Weekday PM Peak Hour Trips (vph)		
		(vpd)	Enter	Exit	Enter	Exit	
Single Family Lots (210)	170 DU	1,644	30	91	103	61	
Townhomes (215)	75 DU	522	8	25	24	17	
Total Trips		2,166	38	116	127	78	

#### **Table 3: Trip Generation Summary**

It is estimated that the proposed development will generate approximately 2,166 total site trips on the roadway network during a typical 24-hour weekday period. Of the daily traffic volume, it is anticipated that 154 trips (38 entering and 116 exiting) will occur during the weekday AM peak hour and 205 trips (127 entering and 78 exiting) will occur during the weekday PM peak hour.

## 4.2. Site Trip Distribution and Assignment

Trip distribution percentages used in assigning site traffic for this development were estimated based on a combination of existing traffic patterns, population centers adjacent to the study area, and engineering judgment.

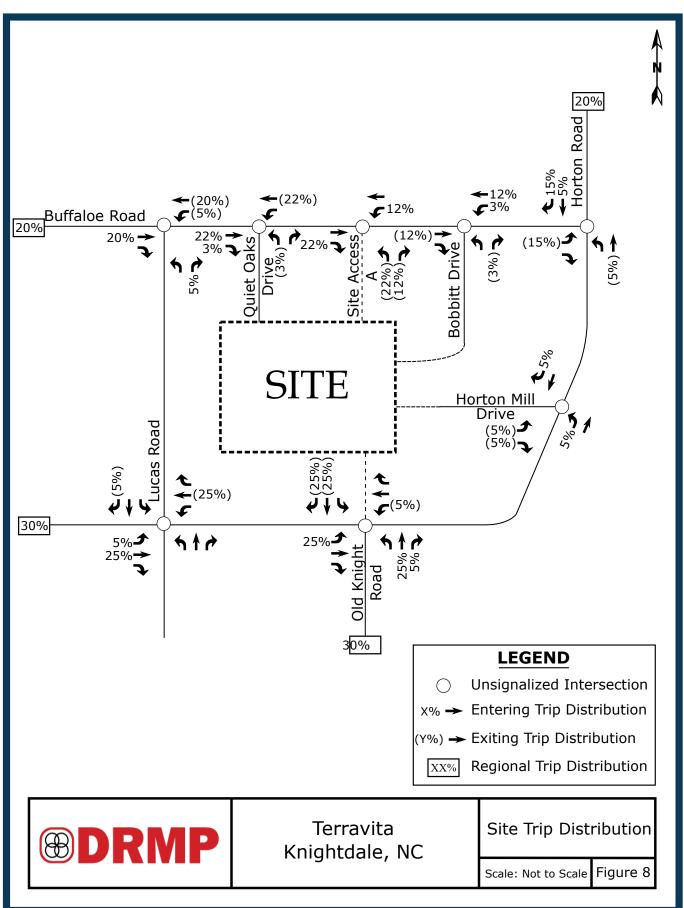
It is estimated that the site trips will be regionally distributed as follows:

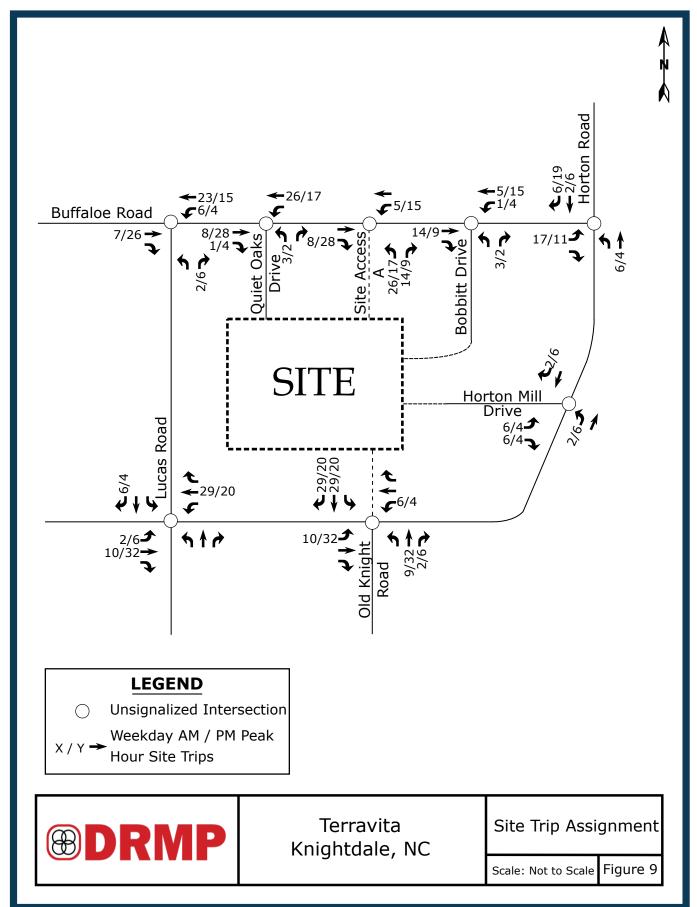
- 30% to/from the south via Old Knight Road
- 30% to/from the west via Horton Road
- 20% to/from the west via Buffaloe Road
- 20% to/from the north via Horton Road

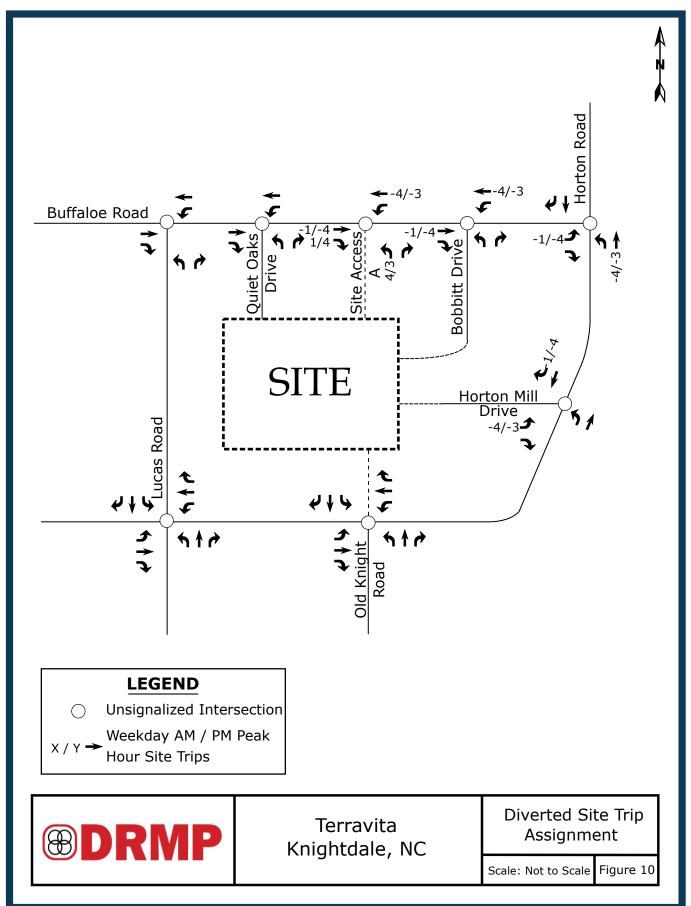


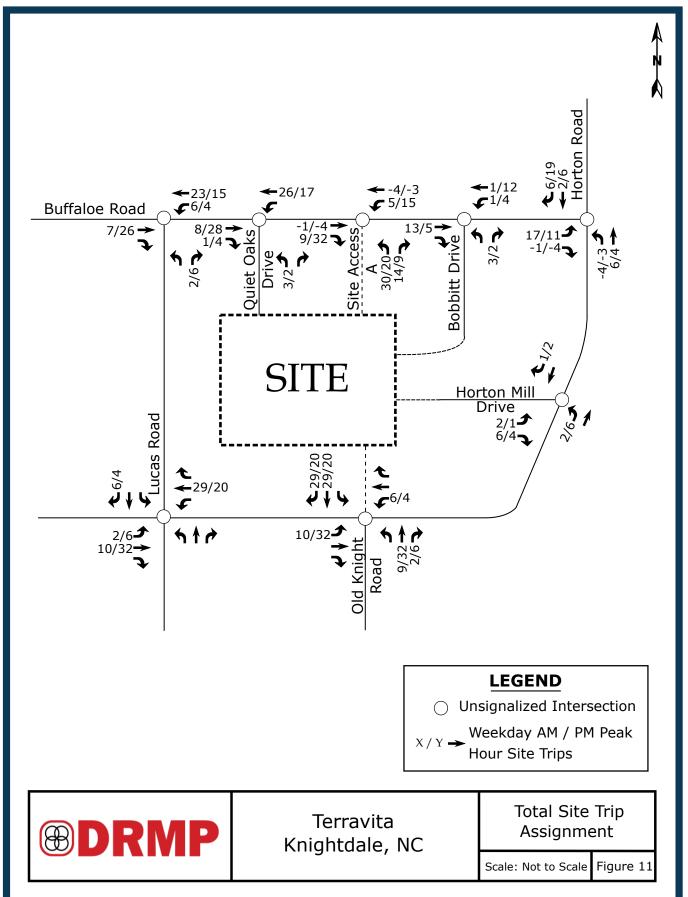
The site trip distribution is shown in Figure 8 and the site trip assignment is shown in Figure 9. Due to connectivity to an adjacent development, some trips are expected to be diverted to use the proposed Site Access. These diverted site trips are shown in Figure 10. The total site trips were determined by adding the site trip assignment and diverted trip assignment together. The total peak hour site trips are shown in Figure 11. It should be noted that the site trip distribution was approved by the Town during scoping.











### 5. BUILD AND FUTURE TRAFFIC CONDITIONS

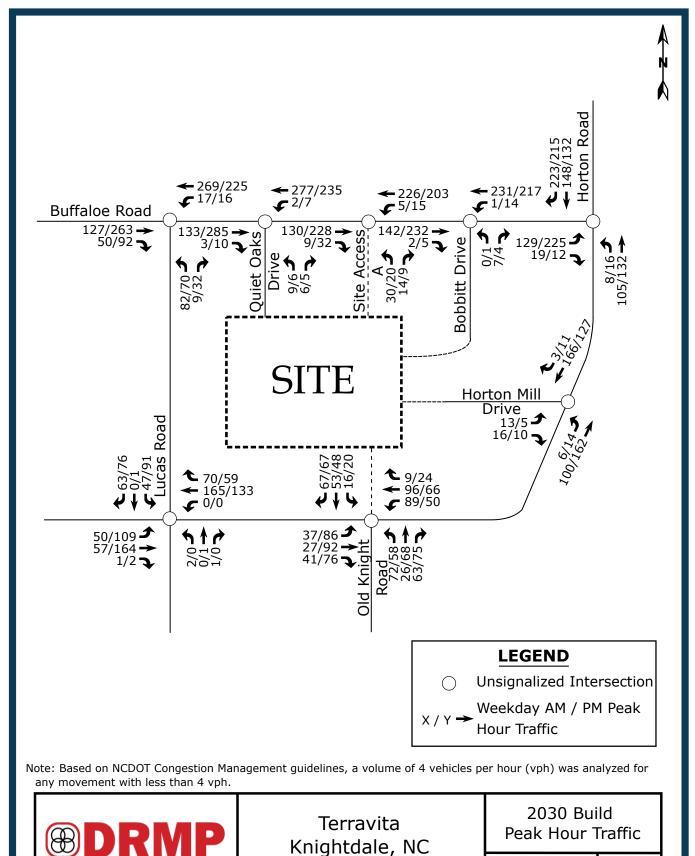
## 5.1. Build and Future Peak Hour Traffic Volumes

To estimate traffic conditions with the site fully built-out, the total site trips were added to the 2030 and 2039 no-build traffic volumes to determine the 2030 build and 2039 future traffic volumes. Refer to Figures 12a and 12b for an illustration of the 2030 build and 2039 future peak hour traffic volumes with the proposed site fully developed.

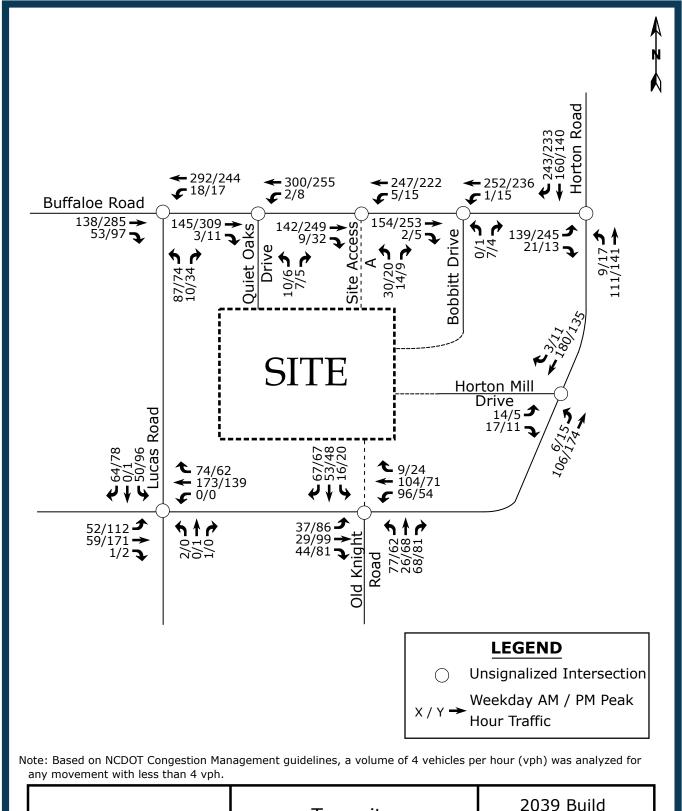
# 5.2. Analysis of Build and Future Peak Hour Traffic Conditions

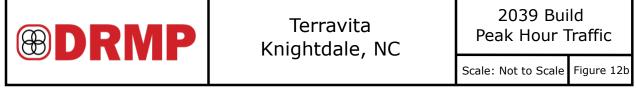
Study intersections were analyzed with the 2030 build and 2039 future traffic volumes using the same methodology previously discussed for existing and no-build traffic conditions. Intersections were analyzed with improvements to accommodate future traffic volumes, if necessary. The results of the capacity analysis for each intersection are presented in Section 7 of this report.





Scale: Not to Scale Figure 12a





## 6. TRAFFIC ANALYSIS PROCEDURE

Study intersections were analyzed using the methodology outlined in the *Highway Capacity Manual* (HCM), 6<sup>th</sup> Edition published by the Transportation Research Board. Capacity and level of service are the design criteria for this traffic study. A computer software package, Synchro (Version 11.1), was used to complete the analyses for the study area intersections. Please note that the unsignalized capacity analysis does not provide an overall level of service for an intersection; only delay for an approach with a conflicting movement.

The HCM defines capacity as "the maximum hourly rate at which persons or vehicles can reasonably be expected to traverse a point or uniform section of a lane or roadway during a given time period under prevailing roadway, traffic, and control conditions." Level of service (LOS) is a term used to represent different driving conditions and is defined as a "qualitative measure describing operational conditions within a traffic stream, and their perception by motorists and/or passengers." Level of service varies from Level "A" representing free flow, to Level "F" where breakdown conditions are evident. Refer to Table 4 for HCM levels of service and related average control delay per vehicle for both signalized and unsignalized intersections. Control delay as defined by the HCM includes "initial deceleration delay, queue move-up time, stopped delay, and final acceleration delay". An average control delay of 50 seconds at a signalized intersection results in LOS "D" operation at the intersection.

UNSIGN	ALIZED INTERSECTION	SIGNALIZED INTERSECTION				
LEVEL OF SERVICE	AVERAGE CONTROL DELAY PER VEHICLE (SECONDS)	LEVEL OF SERVICE	AVERAGE CONTROL DELAY PER VEHICLE (SECONDS)			
A	0-10	А	0-10			
В	10-15	В	10-20			
С	15-25	С	20-35			
D	25-35	D	35-55			
E	35-50	E	55-80			
F	>50	F	>80			

#### Table 4: Highway Capacity Manual – Levels-of-Service and Delay

#### 6.1. Adjustments to Analysis Guidelines

Capacity analysis at all study intersections was completed according to the NCDOT Congestion Management Guidelines.



# 7. CAPACITY ANALYSIS

The following study intersections were analyzed under 2024 existing, 2030 no-build, 2030 build, and 2039 future traffic conditions:

- Buffaloe Road and Lucas Road
- Buffaloe Road and Quiet Oaks Drive
- Buffaloe Road and Bobbitt Drive
- Buffaloe Road and Horton Road
- Horton Road and Horton Mill Drive
- Horton Road and Old Knight Road
- Horton Road and Lucas Road

The proposed site access was analyzed under 2030 build and 2039 future traffic conditions. Refer to Tables 5-12 for a summary of capacity analysis results. Refer to Appendices D-L for the Synchro capacity analysis reports and SimTraffic queueing reports.



## 7.1. Buffaloe Road and Lucas Road

Refer to the table below for a summary of the capacity analysis of the subject intersection during the analysis scenarios.

A P P ANALYSIS R		LANE	ΡΕΑΚ	DAY AM HOUR SERVICE	WEEKDAY PM PEAK HOUR LEVEL OF SERVICE		
SCENARIO	O A C H	CONFIGURATIONS	Approach	Overall (seconds)	Approach	Overall (seconds)	
2024 Existing	EB WB NB	1 TH-RT 1 LT-TH 1 LT-RT	 A (8) <sup>1</sup> B (11) <sup>2</sup>	N/A	 A (8) <sup>1</sup> B (11) <sup>2</sup>	N/A	
2030 No- Build	EB WB NB	1 TH-RT 1 LT-TH 1 LT-RT	 A (8) <sup>1</sup> B (13) <sup>2</sup>	N/A	 A (8) <sup>1</sup> B (14) <sup>2</sup>	N/A	
2030 Build	EB WB NB	1 TH-RT 1 LT-TH 1 LT-RT	 A (8) <sup>1</sup> B (13) <sup>2</sup>	N/A	 A (8) <sup>1</sup> B (14) <sup>2</sup>	N/A	
2039 Future	EB WB NB	1 TH-RT 1 LT-TH 1 LT-RT	 A (8) <sup>1</sup> B (14) <sup>2</sup>	N/A	 A (8) <sup>1</sup> C (15) <sup>2</sup>	N/A	

Table 5: Analysis Summary of Buffaloe Road and Lucas Road

1. Level of service for major-street left-turn movement.

2. Level of service for minor-street approach.

Capacity analysis of all traffic conditions indicates the major street left-turn movement is expected to operate at LOS A during the AM and PM peak hours. Additionally, the minor street approach is expected to operate at LOS C or better during the AM and PM peak hours. No significant queuing is expected at the intersection.



# 7.2. Buffaloe Road and Quiet Oaks Drive

Refer to the table below for a summary of the capacity analysis of the subject intersection during the analysis scenarios.

ANALYSIS	A P P R LANE		WEEKDAY AM PEAK HOUR LEVEL OF SERVICE		WEEKDAY PM PEAK HOUR LEVEL OF SERVICE	
SCENARIO	O A C H	CONFIGURATIONS	Approach	Overall (seconds)	Approach	Overall (seconds)
2024 Existing	EB WB NB	1 TH-RT 1 LT-TH 1 LT-RT	 A (8) <sup>1</sup> A (10) <sup>2</sup>	N/A	 A (8) <sup>1</sup> B (11) <sup>2</sup>	N/A
2030 No- Build	EB WB NB	1 TH-RT 1 LT-TH 1 LT-RT	 A (8) <sup>1</sup> B (10) <sup>2</sup>	N/A	 A (8) <sup>1</sup> B (11) <sup>2</sup>	N/A
2030 Build	EB WB NB	1 TH-RT 1 LT-TH 1 LT-RT	 A (8) <sup>1</sup> B (11) <sup>2</sup>	N/A	 A (8) <sup>1</sup> B (12) <sup>2</sup>	N/A
2039 Future	EB WB NB	1 TH-RT 1 LT-TH 1 LT-RT	 A (8) <sup>1</sup> B (11) <sup>2</sup>	N/A	 A (8) <sup>1</sup> B (12) <sup>2</sup>	N/A

#### Table 6: Analysis Summary of Buffaloe Road and Quiet Oaks Drive

1. Level of service for major-street left-turn movement.

2. Level of service for minor-street approach.

Capacity analysis of all traffic conditions indicates the major street left-turn movement is expected to operate at LOS A during the weekday AM and PM peak hours. Additionally, the minor street approach is expected to operate at an overall LOS B or better during the AM and PM peak hours. No significant queuing is expected at the intersection.



# 7.3. Buffaloe Road and Bobbitt Drive

Refer to the table below for a summary of the capacity analysis of the subject intersection during the analysis scenarios.

ANALYSIS	A P P R LANE		WEEKDAY AM PEAK HOUR LEVEL OF SERVICE		WEEKDAY PM PEAK HOUR LEVEL OF SERVICE	
SCENARIO	O A C H	CONFIGURATIONS	Approach	Overall (seconds)	Approach	Overall (seconds)
2024 Existing	EB WB NB	1 TH-RT 1 LT-TH 1 LT-RT	 A (8) <sup>1</sup> A (10) <sup>2</sup>	N/A	 A (8) <sup>1</sup> B (10) <sup>2</sup>	N/A
2030 No-Build	EB WB NB	1 TH-RT 1 LT-TH 1 LT-RT	 A (8) <sup>1</sup> B (10) <sup>2</sup>	N/A	 A (8) <sup>1</sup> B (11) <sup>2</sup>	N/A
2030 Build	EB WB NB	1 TH-RT 1 LT-TH 1 LT-RT	 A (8) <sup>1</sup> A (10) <sup>2</sup>	N/A	 A (8) <sup>1</sup> B (11) <sup>2</sup>	N/A
2039 Future	EB WB NB	1 TH-RT 1 LT-TH 1 LT-RT	 A (8) <sup>1</sup> B (10) <sup>2</sup>	N/A	 A (8) <sup>1</sup> B (11) <sup>2</sup>	N/A

Table 7: Analysis Summary of Buffaloe Road and Bobbitt Drive

1. Level of service for major-street left-turn movement.

2. Level of service for minor-street approach.

Capacity analysis of all traffic conditions indicates the major street left-turn movement is expected to operate at LOS A during the weekday AM and PM peak hours. Additionally, the minor street approach is expected to operate at an overall LOS B or better during the AM and PM peak hours. No significant queuing is expected at the intersection.



# 7.4. Buffaloe Road and Horton Road

Refer to the table below for a summary of the capacity analysis of the subject intersection during the analysis scenarios.

ANALYSIS	A P P R	LANE	PEAK HOUR PE		PEAK	EEKDAY PM EAK HOUR L OF SERVICE	
SCENARIO	O A C H	CONFIGURATIONS	Approach	Overall (seconds)	Approach	Overall (seconds)	
2024 Existing	EB NB SB	1 LT-RT 1 LT-TH 1 TH-RT	B (11) <sup>2</sup> A (8) <sup>1</sup> 	N/A	B (12) <sup>2</sup> A (8) <sup>1</sup> 	N/A	
2030 No- Build	EB NB SB	1 LT-RT 1 LT-TH 1 TH-RT	B (13) <sup>2</sup> A (8) <sup>1</sup> 	N/A	C (16) <sup>2</sup> A (8) <sup>1</sup> 	N/A	
2030 Build	EB NB SB	1 LT-RT 1 LT-TH 1 TH-RT	B (13) <sup>2</sup> A (8) <sup>1</sup> 	N/A	C (17) <sup>2</sup> A (8) <sup>1</sup> 	N/A	
2039 Future	EB NB SB	1 LT-RT 1 LT-TH 1 TH-RT	B (14) <sup>2</sup> A (8) <sup>1</sup> 	N/A	C (19) <sup>2</sup> A (8) <sup>1</sup> 	N/A	

**Table 8: Analysis Summary of Buffaloe Road and Horton Road** 

1. Level of service for major-street left-turn movement.

2. Level of service for minor-street approach.

Capacity analysis of all traffic conditions indicates the major street left-turn movement is expected to operate at LOS A during the weekday AM and PM peak hours. Additionally, the minor street approach is expected to operate at an overall LOS C or better during the AM and PM peak hours. No significant queuing is expected at the intersection.



## 7.5. Horton Road and Horton Mill Drive

Refer to the table below for a summary of the capacity analysis of the subject intersection during the analysis scenarios.

ANALYSIS	A P P R	LANE	WEEKD PEAK H LEVEL OF		WEEKD PEAK LEVEL OF	HOUR
SCENARIO	O A C H	CONFIGURATIONS	Approach	Overall (seconds)	Approach	Overall (seconds)
2024 Existing	EB NB SB	1 LT-RT 1 LT-TH 1 TH-RT	A (9) <sup>2</sup> A (8) <sup>1</sup> 	N/A	A (9) <sup>2</sup> A (7) <sup>1</sup> 	N/A
2030 No- Build	EB NB SB	1 LT-RT 1 LT-TH 1 TH-RT	A (10) <sup>2</sup> A (8) <sup>1</sup> 	N/A	A (10) <sup>2</sup> A (8) <sup>1</sup> 	N/A
2030 Build	EB NB SB	1 LT-RT 1 LT-TH 1 TH-RT	A (10) <sup>2</sup> A (8) <sup>1</sup> 	N/A	A (10) <sup>2</sup> A (8) <sup>1</sup> 	N/A
2039 Future	EB NB SB	1 LT-RT 1 LT-TH 1 TH-RT	B (10) <sup>2</sup> A (8) <sup>1</sup> 	N/A	A (10) <sup>2</sup> A (8) <sup>1</sup> 	N/A

#### **Table 9: Analysis Summary of Horton Road and Horton Mill Drive**

1. Level of service for major-street left-turn movement.

2. Level of service for minor-street approach.

Capacity analysis of all traffic conditions indicates the major street left-turn movement is expected to operate at LOS A during the weekday AM and PM peak hours. Additionally, the minor street approach is expected to operate at an overall LOS B or better during the AM and PM peak hours. No significant queuing is expected at the intersection.



# 7.6. Horton Road and Old Knight Road

Refer to the table below for a summary of the capacity analysis of the subject intersection during the analysis scenarios.

ANALYSIS SCENARIO	A P P R LANE		WEEKDAY AM PEAK HOUR LEVEL OF SERVICE		WEEKDAY PM PEAK HOUR LEVEL OF SERVICE	
	O A C H		Approach	Overall (seconds)	Approach	Overall (seconds)
2024 Existing	EB WB NB	1 TH-RT 1 LT-TH 1 LT, 1 RT	 A (7) <sup>1</sup> A (10) <sup>2</sup>	N/A	 A (8) <sup>1</sup> A (9) <sup>2</sup>	N/A
2030 No-Build	EB WB NB SB	<u>1 LT</u> , 1 TH-RT 1 LT-TH- <u>RT</u> 1 LT- <u>TH</u> , 1 RT <u>1 LT-TH-RT</u>	A (8) <sup>1</sup> A (8) <sup>1</sup> B (13) <sup>2</sup> B (12) <sup>2</sup>	N/A	A (8) <sup>1</sup> A (8) <sup>1</sup> B (13) <sup>2</sup> B (13) <sup>2</sup>	N/A
2030 Build	EB WB NB SB	<u>1 LT</u> , 1 TH-RT 1 LT-TH- <u>RT</u> 1 LT- <u>TH</u> , 1 RT <u>1 LT-TH-RT</u>	A (8) <sup>1</sup> A (8) <sup>1</sup> B (15) <sup>2</sup> B (13) <sup>2</sup>	N/A	A (8) <sup>1</sup> A (8) <sup>1</sup> C (17) <sup>2</sup> B (15) <sup>2</sup>	N/A
2039 Future	EB WB NB SB	<u>1 LT</u> , 1 TH-RT 1 LT-TH- <u>RT</u> 1 LT- <u>TH</u> , 1 RT <u>1 LT-TH-RT</u>	A (8) <sup>1</sup> A (8) <sup>1</sup> C (15) <sup>2</sup> B (14) <sup>2</sup>	N/A	A (8) <sup>1</sup> A (8) <sup>1</sup> C (18) <sup>2</sup> C (16) <sup>2</sup>	N/A

#### Table 10: Analysis Summary of Horton Road and Old Knight Road

Improvements to lane configurations by adjacent development are shown underlined.

1. Level of service for major-street left-turn movement.

2. Level of service for minor-street approach.

Capacity analysis of all traffic conditions indicates the major street left-turn movements are expected to operate at LOS A during the weekday AM and PM peak hours. Additionally, the minor street approaches are expected to operate at an overall LOS C or better during the AM and PM peak hours. No significant queuing is expected at the intersection.

Under no-build conditions, the Weldon Village adjacent development is expected to construct the southbound approach at the intersection and construct an eastbound left turn lane with 100 feet of storage plus appropriate deceleration and taper. The Weldon Village connection with provide indirect connectivity to the proposed development. No additional improvements are recommended by the developer.



# 7.7. Horton Road and Lucas Road

Refer to the table below for a summary of the capacity analysis of the subject intersection during the analysis scenarios.

ANALYSIS SCENARIO	A P P R LANE		WEEKDAY AM PEAK HOUR LEVEL OF SERVICE		WEEKDAY PM PEAK HOUR LEVEL OF SERVICE	
	O A C H	CONFIGURATIONS	Approach	Overall (seconds)	Approach	Overall (seconds)
2024 Existing	EB WB NB SB	1 LT-TH-RT 1 LT-TH-RT 1 LT-TH-RT 1 LT-TH-RT	A (8) <sup>1</sup> A (7) <sup>1</sup> A (10) <sup>2</sup> A (10) <sup>2</sup>	N/A	A (8) <sup>1</sup> A (7) <sup>1</sup> A (10) <sup>2</sup> B (10) <sup>2</sup>	N/A
2030 No-Build	EB WB NB SB	1 LT-TH-RT 1 LT-TH-RT 1 LT-TH-RT 1 LT-TH-RT 1 LT-TH-RT	A (8) <sup>1</sup> A (7) <sup>1</sup> B (11) <sup>2</sup> B (11) <sup>2</sup>	N/A	A (8) <sup>1</sup> A (8) <sup>1</sup> B (13) <sup>2</sup> C (15) <sup>2</sup>	N/A
2030 Build	EB WB NB SB	1 LT-TH-RT 1 LT-TH-RT 1 LT-TH-RT 1 LT-TH-RT	A (8) <sup>1</sup> A (7) <sup>1</sup> B (12) <sup>2</sup> B (12) <sup>2</sup>	N/A	A (8) <sup>1</sup> A (8) <sup>1</sup> B (14) <sup>2</sup> C (17) <sup>2</sup>	N/A
2039 Future	EB WB NB SB	1 LT-TH-RT 1 LT-TH-RT 1 LT-TH-RT 1 LT-TH-RT 1 LT-TH-RT	A (8) <sup>1</sup> A (7) <sup>1</sup> B (12) <sup>2</sup> B (12) <sup>2</sup>	N/A	A (8) <sup>1</sup> A (8) <sup>1</sup> B (14) <sup>2</sup> C (18) <sup>2</sup>	N/A

Table 11: Analysis Summary of Horton Road and Lucas Road

1. Level of service for major-street left-turn movement.

2. Level of service for minor-street approach.

Capacity analysis of all traffic conditions indicates the major street left-turn movements are expected to operate at LOS A during the weekday AM and PM peak hours. Additionally, the minor street approaches are expected to operate at an overall LOS C or better during the AM and PM peak hours. No significant queuing is expected at the intersection.



## 7.8. Buffaloe Road and Site Access

Refer to the table below for a summary of the capacity analysis of the subject intersection during the analysis scenarios.

ANALYSIS	A P P R	LANE	WEEKDAY AM PEAK HOUR LEVEL OF SERVICE		WEEKDAY PM PEAK HOUR LEVEL OF SERVICE	
SCENARIO	O A C H	CONFIGURATIONS	Approach	Overall (seconds)	Approach	Overall (seconds)
2030 Build	EB WB <b>NB</b>	1 TH- <b>RT</b> 1 <b>LT</b> -TH 1 <b>LT-RT</b>	 A (8) <sup>1</sup> B (11) <sup>2</sup>	N/A	 A (8) <sup>1</sup> B (12) <sup>2</sup>	N/A
2039 Future	EB WB <b>NB</b>	1 TH- <b>RT</b> 1 <b>LT</b> -TH 1 <b>LT-RT</b>	 A (8) <sup>1</sup> B (11) <sup>2</sup>	N/A	 A (8) <sup>1</sup> B (12) <sup>2</sup>	N/A

**Table 12: Analysis Summary of Buffaloe Road and Site Access** 

Modifications to lane configurations by developer are shown in bold.

1. Level of service for major-street left-turn movement.

2. Level of service for minor-street approach.

Capacity analysis of all the 2030 build and 2039 traffic conditions indicates the major street left-turn movement is expected to operate at LOS A during the weekday AM and PM peak hours. Additionally, the minor street approach is expected to operate at an overall LOS B or better during the AM and PM peak hours. No significant queuing is expected at the intersection.

Turn lanes along Buffaloe Road at the proposed Site Access were considered based on the NCDOT *Policy on Street and Driveway Access to North Carolina Highways*, but are not warranted based on peak hour volumes. Sight distance appears to be sufficient along Buffaloe Road at the proposed access location. As typical, actual sight distances will be measured and verified in the field as part of the driveway permitting process. No improvements are recommended by the developer.



## 8. CONCLUSIONS

This Traffic Impact Analysis was conducted to determine the potential traffic impacts of the Terravita development to be located south of Buffaloe Road between Quiet Oaks Drive and Bobbitt Drive in Knightdale, North Carolina. The proposed development, anticipated to be completed in 2029, is assumed to consist of 170 single-family homes and 75 townhomes. Site access is proposed via one (1) new full movement driveway along Buffaloe Road and internal connections to Quiet Oaks Road, Bobbitt Drive, Proc Ridge Lane, and the Old Knight Road extension (a part of the Weldon Village adjacent development).

The study analyzes traffic conditions during the weekday AM and PM peak hours for the following scenarios:

- 2024 Existing Traffic Conditions
- 2030 No-Build (build year+1) Traffic Conditions
- 2030 Build (build year+1) Traffic Conditions
- 2039 Future (build year+10) Traffic Conditions

#### Trip Generation

It is anticipated that proposed development will generate 154 total trips (38 entering and 116 exiting) during the weekday AM peak hour and 205 total trips (127 entering and 78 exiting) during the weekday PM peak hour.

#### Adjustments to Analysis Guidelines

Capacity analysis at all study intersections was completed according to NCDOT Congestion Management Guidelines.



## 9. **RECOMMENDATIONS**

Based on the findings of this study, no specific geometric improvements have been identified to accommodate future traffic conditions. See a more detailed description of the recommended modifications below. Refer to Figure 13 for an illustration of the recommended lane configuration for the proposed development.

#### Improvements by Weldon Village

Horton Road and Old Knight Road

- Construct southbound approach (of Old Knight Road) with one ingress lane and one egress lane.
- Provide stop control for southbound approach.
- Construct eastbound left turn lane (on Horton Road) with 100' of storage plus appropriate deceleration and taper.

#### **Recommended Modifications by Developer**

#### Buffaloe Road and Site Access

• Construct northbound approach (of the proposed site access) with one ingress lane and one egress lane. Provide stop-control for the northbound approach.



